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Dear Dr. Machta:

This is in further reply to your letter of 7 July. I have read your report with a great deal of interest and I do not think that there is any undue overlap between the two lines of attack that we are following. Enclosed is a brief report (prepared for the Castle Report) on a simplified version of our procedure. With regard to the further study mentioned in paragraph two, the following remarks on other items in the enclosure will give you a pretty good idea of what we are trying to do on the IBM Model 701 Computer.

- 3 (a) The initial cloud may be subdivided into any number of horizontal slices within reason. The central concentration may be any arbitrary function of altitude.
- (c)  $a_0$  may be any function of altitude.
- (d) Radioactivity is normally distributed with respect to the logarithm of the rate of fall of particles. (We are currently assuming that the rate of fall of any given particle does not change with altitude.)
- (e) The power law of diffusion may be taken as different from the square law.  $S$  is the total distance (instead of horizontal distance) traveled by the central particle. The ratio of  $S$  to  $S_0$  is taken as a parameter that is independent of altitude.

Our intention is to vary these parametric quantities in order to obtain the best agreement between observed and calculated fall-out, and to assess the relative importance of the various parameters in the hope of obtaining a better simplified method that will be suitable for operational use. At the present time we are concentrating at the time of the Bravo distant fall-out from Operation Castle. We will soon have to give attention to the local Castle fall-out and will then probably find it necessary to make some allowance, as you have done, for the effect of winds during the formation of the "initial cloud".

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Lester Machta

19 August 1954

I hope that we may have an opportunity to get together soon for a conference on this general problem.

Yours very sincerely,

THOMAS H. WHITE, Leader  
Radiological Physics Group  
Health Division

Thn/ek

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Radioactive Fall-out

A Proposed Method for Isolating, in the Estimation of the Formation  
of Radioactive Particles such as are found in an Atomic Bomb Cloud  
(Written by T. J. White for the Radiological safety feasibility study)

1. Introduction

1.1 Recent tests at AFB have made it apparent that radio-active fall-out on distant communities place certain rather serious limitations on the use of the Proving Ground. Towards the end of the trials, in a single series of shots, those who had given most thought to the problem concluded that there is one factor that predominates in determining the intensity of fall-out. This factor is the proximity of the fire-ball to the ground. The evidence is very strong that if the fire-ball makes extensive contact with the ground, the fall-out will be heavy, and that if the fire-ball remains definitely clear of the ground the fall-out will be light. It seems with good fire ball contact the radiation intensities from the material deposited on the ground will be several orders of magnitude greater than the intensities observed following a shot with no contact. It appears that this factor is much more dependent upon bomb yield (except insofar as this affects fire-ball radius) on meteorological conditions (although these are of great importance in determining whether fall-out will occur).

1.2 There is also a certain amount of evidence indicating that some very special conditions are necessary for the formation of a radioactive fall-out particle. For example, it appears that all of the particles of dirt that fall from the cloud formed by a low altitude, direct hit, 150 kiloton explosion contain radio-active material. In the opinion of some observers, these radioactive particles always have the appearance of having been forced to fly a greater or lesser extent. Other observers have found it impossible to distinguish between active and inactive particles on the basis of appearance under the microscope. However this may

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be, it is usually noticed that heavy fall-out from NPG shots is associated with considerable fusing of the earth around ground zero.

1.3 Of several methods of model stabilizers that have been tried, none has had any notable effect on the intensity of fall-out from tower shots. It seems somewhat doubtful if any satisfactory device can be found. If one could be found that would also facilitate subsequent identification of a tower-shot area, it would be useful even though it may possibly be expensive in comparison with, for example, Aspinwall. The cost of considerable experimenting in the field tests is very great.

1.4 Even if no satisfactory method of reducing fall-out from tower shots can be found, there is much to be learned by investigation of the mechanism of production of the active fall-out particles in order to improve the confidence of predictions. The process of gathering information from various ground tests is much too slow, provides little information on the effects of the most important factor - burst height - in the critical range, and suffers from limitations on account of incomplete fall-out cover along with many other variables.

1.5 For these reasons it is felt urgent here for a laboratory method of investigating the mechanism. It occurred to the writer that an electric arc might have certain properties enough like those of a fire-ball to be used as a tool for investigating the mechanism up to a laboratory scale.

1.6 In Section I are set forth certain possibilities that appear to be necessary in order that a laboratory model might have some hope of providing useful information. The remaining Sections and Appendices discuss topics preliminary to experimental trials. It is intended to proceed with the preliminary experiments within H-6. If these experiments show the model to be promising, it may be necessary to ask for assistance from other groups, e.g. for high-speed photography.

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It is the writer's opinion that if the method is to give useful results, it should be pursued vigorously on a co-operative basis.

2. General Similarity Requirements - Characteristics:

2.1 In order to have an instructive laboratory model, it appears that the following conditions must be met:

- a. The "fire-ball" must be capable of rapidly heating a sandy surface with which it can contact for a time of the order of a few seconds.
- b. The production of the "fire-ball" must be sufficiently sudden and violent so that a large volume must be blown up, and sucked up towards the "fire-ball" even when the "fire-ball" does not contact the surface. This is needed to provide mass anchorage for the "air-burst" phenomena.
- c. The "fire-ball" must contain suspended or finely dispersed radioactive material capable of attachment to fine particles under unknown conditions, probably high temperature conditions.
- d. The "fire-ball" should however be able to then rise quite rapidly, without excessive dispersal. When it rises as to contact a dusty surface, it must carry a perceptible amount of dust up with it. It is not essential that it should be capable of carrying up particles as large as 100 microns (typical sand particle size), but it should be able to carry up particles that are small enough to fall back to the "ground" in a reasonable length of time (preferably less than one hour). This is expected so that it may be possible to distinguish "fall-out" activity from activity deposited by condensation or adhesion on the surface.
- e. Other conditions may also be present. In addition to the above. Some similarity in the relationships of temperature, energy, and volume, with time, may be needed. However, it seems that there is not much chance

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of producing a useful fire-ball without the first four conditions can be met.

### 3. Consideration of Thermal Shock

For elevation of cutting by thermal shock, prior to a rival of the blast wave, we need to deliver  $\epsilon_{\text{heat}} \text{ cal/cm}^2$  in a time  $t = b/v$ , where  $b$  is the height of the fire-ball above ground, and  $v$  is the initial shock velocity over this distance.

Radiation rate  $\epsilon = \sigma T^4 (r/a)^2$  (EAW, 1959)

$$\epsilon = \frac{\sigma}{8} \int_0^R r_a(t) v^4(t) r^2(t) dr$$

If we assume  $T$  const. at  $T = 10^3^\circ\text{K}$ ,  $r_a = R_a = R$ ,

$v = 3 \times 10^4 \text{ cm/sec}$  (minimum value)  $\approx 10 \text{ cm/sec}$ .

$$\epsilon = \frac{\sigma}{8} \int_0^R r^2 v^2 \times 1.2 \text{ hr} = 0.000001 \frac{\text{cal}}{\text{cm}^2}$$

$$\frac{r^2}{v^2} = \frac{0.00001}{0.00001} = \frac{10^8}{(3 \times 10^4)^2} \approx 5000 \text{ cm.}$$

Under these assumptions, the heat emitted is delivered before the shock arrives.

We need to consider the variation of  $\epsilon$  to find out if  $\epsilon$  can exceed  $3 \times 10^6$

$T$	$10^{-12} T^4$	$r_a$	$\epsilon_{\text{heat}} \text{ cal/cm}^2 \times 10^{12}$	
$10^4$	$10^4$	1	$10^4$	
$2 \cdot 10^4$	$16 \cdot 10^4$	1	$5 \cdot 10^4$	
$5 \cdot 10^4$	$6 \cdot 10^6$	1	$6 \cdot 10^5$	
$7 \cdot 10^4$	$2.5 \times 10^7$	1	$2 \cdot 10^6$	Apparently a temperature of the order of $10^5^\circ\text{K}$ is needed.
$12 \cdot 10^4$	$2 \times 10^8$	1	$2 \cdot 10^6$	
$30 \cdot 10^4$	$8 \times 10^9$	1	$8 \times 10^6$	

(from EAW)

Further, it appears that a given thermal load of  $10 \text{ cal/cm}^2$  can occur only under circumstances where the fire-ball does not touch the ground. From EAW:

Distance (m)       $\epsilon_{\text{heat}} \text{ cal/cm}^2 \text{ in } 10^{-3} \text{ sec}$

1	$10^2$
10	$10^2$
100	10

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If  $d$  is the diameter of a particle in microns, then the elevation in temperature from 10 cal/cm<sup>2</sup> is of the order of  $10^4/d^2$ . It appears that particles less than  $\sim 10 \mu$  could be melted.

#### 4. Notes on Arc Requirements

4.1 Suppose that an arc is produced by the discharge of a condenser thru an otherwise non-resistive circuit.

Energy discharged =  $C/V^2$  coulombs

$$= \frac{C}{2} \cdot \frac{V^2}{2} \text{ cal}$$

If 1% is radiated, the energy /cm<sup>2</sup> at distance  $r$  cm is

$$\frac{C}{2} \times \frac{10^{-4}}{4\pi r^2} \cdot \frac{V^2}{2} \text{ cal/cm}^2$$

$$\approx 10^{-6} \frac{V^2}{r^2}$$

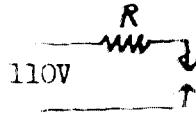
To get 1 cal/cm<sup>2</sup> at 1 cm distance we need

$$CV^2 = 10^6 \text{ coulombs}$$

e.g. 1 farad charged to 1000 volt.

#### IMPERFECT ARCS

4.2

  
110V       $\frac{R}{L}$       Arc gap  $G$  rec.  
                 $\uparrow$       30 amp, 55 volt,  
I giving  $\approx 1600$  joules,  $1000 \text{ cm}^2$ ,  $10^6$  cal  
in radiation at 10 cm from the point of distance.

This should do for a first try.

#### 4.3 High-current carbon arc references:

Finkelnburg, J. App. Physics 21, 149 (1950) describes steady state characteristics as compared with low-current 1 amp. Notching characteristics.

Phys. Rev. 80, 243 (1950) Measurements to complete the theory.

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#### 4.4 Initiation of Arcs

Brit. J. App. Physic., 2, 271 (1951) gives a starting circuit, somewhat complicated, useful for long term problems.

#### 5. Alternative Method

There may be some advantage in using a short-circuiting wire (fuse effect) instead of an arc. It would seem that, for a given final temperature attained (well above the boiling point of the metal) the initial pressure shock might be greater. The intuitive argument favoring this view is that, with a given volume to start with, the final final temperature reached in the metal would be greater simply because the initial energy would be just 1/6.4 times greater. A larger "fire-ball" would be produced from the same initial volume of energy. Also the fuse method would ensure that the fire-ball would be rich in metal from the earliest stages. In fact if the energy can be pumped in fast enough, the mechanism might be just like that of the pump fire-ball growth mechanism.

Did Kapitza publish anything except his experiments on exploding wires by short-circuiting big generators? Look up for example the references given by 621.3178 L37e on fuse theory.

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